

# Effect of a GW on an interferometer in the TT gauge

We consider the ~~detector~~ (at least) ~~interferometer~~ plane (~~the test mass is free~~) ~~in the~~ the TT gauge.

Let's imagine that a GW with polarization + propagates along the axe 2. It is not important the direction because the only relevant fact is the value of  $h$  on the plane where the test moves are located ( $z=0$ ). The Michelson interferometer has the arms along the  $x$  and  $y$  axes.

For 2 events separated by an infinitesimal distance on the detector plane we have

$$ds^2 = -c^2 dt^2 + [1+h_+(t)] dx^2 + [1-h_+(t)] dy^2 \quad (1)$$

$t, x$ , and  $y$  are the coordinates as seen by the observer using ~~the~~ the TT gauge.

A photon has  $ds^2 = 0$ .

(2)

For a photon that propagates along the x-axis:

$$c^2 dt^2 = [1 + h_+] dx^2 \quad (2)$$

which means  $dt \approx \pm \left[ 1 + \frac{h_+}{2} \right] \frac{dx}{c}$  (3) considering that  $h_+ \ll 1$ . + is for ~~waves~~ photons travelling right bound whereas - is for left bound photons.

Let's calculate the time the photon takes to go to the mirror and come back.

$$\begin{aligned} t_2 - t_0 &= t_2 - t_1 + t_1 + t_0 = \int_{t_0}^{t_1} dt + \int_{t_1}^{t_2} dt = \\ &= \int_0^{L_x} \left[ 1 + \frac{h_+}{2} \right] \frac{dx}{c} - \int_{L_x}^0 \left[ 1 + \frac{h_+}{2} \right] \frac{dx}{c} = \frac{2L_x}{c} + \int_0^{L_x} dx - \int_{L_x}^0 dx \end{aligned}$$

Now a trick: from (3), to 0-order in  $h$ ,  $\frac{dx}{c} = \pm dt$

hence :

~~$$t_2 - t_0 = \int_{t_0}^{L_x/c} \left[ 1 + \frac{h_+}{2} \right] dt \mp \int_{L_x/c}^0 \left[ 1 + \frac{h_+}{2} \right] dt$$~~

The position  $L_x$  of the mirror does not change because we are in the  $TT$  gauge

$$t_2 - t_0 = \frac{2L_x}{c} + \frac{1}{2} \int_{t_0}^{L_x/c} h_+(t) dt + \frac{1}{2} \int_{L_x/c}^0 h_+(t) dt = \frac{L_x}{c}$$

(3)

$$= \frac{2Lx}{c} + \frac{1}{2} \int_{t_0}^{t_2} h_+(t) dt = \frac{2Lx}{c} + \frac{1}{2} h_0 \int_{t_0}^{t_2} \sin(\Omega t) dt$$

$$t_2 - t_0 = \frac{2Lx}{c} + \frac{h_0}{2\Omega} [\omega_s(\Omega t_0) - \omega_s(\Omega t_2)] \quad (4)$$

at 0-order in  $h$  we have  $t_2 = t_0 + \frac{2Lx}{c}$  hence :

$$t_2 - t_0 = \frac{2Lx}{c} + \frac{h_0}{2\Omega} [\omega_s(\Omega t_0) - \omega_s\{\Omega[t_0 + \frac{2Lx}{c}]\}]$$

$$\begin{aligned} \omega_s d - \cos(\alpha + 2\beta) &= \cos d - \cos d \cos 2\beta + \sin d \sin 2\beta = \\ &= \cos d (1 - \cos^2 \beta) + \sin d \sin 2\beta = 2 \cos d \sin^2 \beta + 2 \sin d \sin \beta \cos \beta = \\ &= 2 \sin \beta (\cos d \sin \beta + \sin d \cos \beta) = 2 \sin \beta \sin(d + \beta) \end{aligned}$$

Hence :

$$\begin{aligned} t_2 - t_0 &= \frac{2Lx}{c} + \frac{h_0}{\Omega} \sin\left[\Omega\left(t_0 + \frac{Lx}{c}\right)\right] \cdot \sin\left(-\Omega \frac{Lx}{c}\right) = \\ &= \frac{2Lx}{c} \left\{ 1 + \frac{h_0}{2} \sin\left[\Omega\left(t_0 + \frac{Lx}{c}\right)\right] \cdot \frac{\sin\left(-\Omega \frac{Lx}{c}\right)}{\Omega \frac{Lx}{c}} \right\} \end{aligned} \quad (5)$$

(4)

the previous equation needs to be explained a bit.  
 $t_0$  and  $t_2$  are 2 running times, one linked to  
 the beam splitter when the beam departs and the  
 other,  $t_2$ , linked to the BS when the beam arrives.

At the departure time the electric field is  $\vec{E}_0 e^{-i\omega t_0}$

At the arrival time the electric field is  $\frac{\vec{E}_0}{2} e^{-i\omega t_2}$

The MM book decided to work with the arrival time  
 then the electric field then :

$$\vec{E}^{(x)}(t) = \frac{\vec{E}_0}{2} e^{-i\omega t_0(t)} = \frac{\vec{E}_0}{2} e^{-i\omega\left\{t - \frac{2Lx}{c}\right\}} + \frac{h_0}{\Omega} \sin\left[\Omega\left(t - \frac{Lx}{c}\right)\right] \sin\frac{\pi Lx}{c}$$
(6)

where we made the replacement of  $t_2$  with  $t$   
 and, to zero order in  $h$ , we have  $t_2 = t = t_0 + \frac{2Lx}{c}$

The previous can be written as :

$$\vec{E}^{(x)}(t) = \frac{\vec{E}_0}{2} e^{-i\left\{\omega\left(t - \frac{2Lx}{c}\right) - \delta\varphi^{(x)}\right\}}$$
(7)

where  $\delta\varphi^{(x)} = \frac{\omega}{\Omega} h \left(t - \frac{Lx}{c}\right) \cdot \sin\left(\frac{\Omega Lx}{c}\right)$

(8)

(5)

With similar arguments we have

$$\vec{E}^{(y)}(t) = -\frac{\vec{E}_0}{2} e^{-i\left\{\omega(t-\frac{2L_y}{c}) + \delta\varphi^{(y)}\right\}} \quad (9)$$

where  $\delta\varphi^{(y)} = \frac{\omega}{\Omega} h(t - \frac{L_y}{c}) \cdot \sin\left(\Omega \frac{L_y}{c}\right)$  (10)

So, the electric field leaving the BS towards the photodiode is :

$$\vec{E}_{\text{out}} = \frac{\vec{E}_0}{2} \left\{ e^{-i\left[\omega(t-\frac{2L_x}{c}) + \delta\varphi^{(x)}\right]} - e^{-i\left[\omega(t-\frac{2L_y}{c}) + \delta\varphi^{(y)}\right]}\right\} \quad (11)$$

The intensity is proportional to  $\vec{E}^* \cdot \vec{E}$ .

$$\begin{aligned} I \propto \vec{E}_{\text{out}} \cdot \vec{E}_{\text{out}}^* &= \frac{E_0^2}{4} \left\{ 1 + 1 + \right. \\ &\quad - e^{-i\left[\omega \frac{2(L_y-L_x)}{c} - \delta\varphi^{(x)} - \delta\varphi^{(y)}\right]} + \\ &\quad \left. - e^{+i\left[\omega \frac{2(L_y-L_x)}{c} - \delta\varphi^{(x)} - \delta\varphi^{(y)}\right]}\right\} = \\ &= \frac{E_0^2}{2} \left\{ 1 - \cos\left[\omega \frac{2(L_y-L_x)}{c} - \delta\varphi^{(x)} - \delta\varphi^{(y)}\right]\right\} \end{aligned}$$

The length difference is small compared to the lengths, so: (12)

$$L_y - L_x = \Delta L \ll L_x, L_y \rightarrow \delta\varphi^{(x)} + \delta\varphi^{(y)} = 2\delta\varphi = 2 \frac{\omega}{\Omega} h_0 \sin\left(t - \frac{L}{c}\right) \sin\left(\frac{\Omega L}{c}\right)$$

$$I \propto \frac{E_0^2}{2} \left\{ 1 - \cos [\varphi_0 - 2\delta\varphi] \right\}$$

$$\delta\varphi = \frac{\omega}{\Omega} h_0 \cdot \sin \left[ \left( t - \frac{L}{c} \right) \right] \sin \left( \frac{\Omega L}{c} \right)$$

$$\delta\varphi \sim \frac{10^{14}}{10^2} \cdot 10^{-21} = 10^{-9} \text{ rad.} \ll 1 \text{ then}$$

$$I \propto \frac{E_0^2}{2} \left\{ 1 - \cos \varphi_0 - \sin \varphi_0 \cdot 2\delta\varphi \right\} \quad (13)$$

It seems better to have  $\varphi_0 = \frac{\pi}{2}$  but the DC is huge!

Instead, if  $\varphi_0$  is close to 0 we can write:

$$I \propto \frac{E_0^2}{2} \left\{ 1 - 1 + \frac{\varphi_0^2}{2} - \varphi_0 \cdot 2\delta\varphi \right\}$$

Hence, the signal-to-DC ratio is  $\frac{2\delta\varphi}{\varphi_0}$

If one consider the signal-to-noise ratio, the main source of noise is the shot noise, which is proportional to the square root of the intensity  $\rightarrow I_{\text{shot}} \propto \varphi_0$   
hence the SNR become constant for  $\varphi_0 \rightarrow 0$ .